

Module 3d: Flow in Pipes Manning's Equation

Robert Pitt
University of Alabama
and
Shirley Clark
Penn State - Harrisburg

Manning's Equation

- Manning's Equation for velocity and flow applicable to both pipe (closed-conduit) flow and open channel flow.
- It is typically applied only in open-channel flow (fluid in contact with atmosphere).

Manning's Equation

- For Fluid Velocity in U.S. Customary Units:

$$V = \frac{1.486R^{2/3}S^{1/2}}{n}$$

Where V = velocity (ft/sec)
R = hydraulic radius (ft)
S = slope of the energy grade line
n = Manning's roughness coefficient

Manning's Equation

- For Fluid Velocity in SI Units:

$$V = \frac{R^{2/3}S^{1/2}}{n}$$

Where V = velocity (m/sec)
R = hydraulic radius (m)
S = slope of the energy grade line
n = Manning's roughness coefficient

Manning's Equation: n Values

| Surface | Best | Good | Fair | Bad |
|--|-------------|-------|-------|-------|
| Uncoated cast-iron pipe | 0.012 | 0.013 | 0.014 | 0.015 |
| Coated cast-iron pipe | 0.011 | 0.012 | 0.013 | |
| Commercial wrought-iron pipe, black | 0.012 | 0.013 | 0.014 | 0.015 |
| Commercial wrought-iron pipe, galvanized | 0.013 | 0.014 | 0.015 | 0.017 |
| Smooth brass and glass pipe | 0.009 | 0.010 | 0.011 | 0.013 |
| Smooth lockbar and welded "OD" pipe | 0.010 | 0.011 | 0.013 | |
| Vitrified sewer pipe | 0.010/0.011 | 0.013 | 0.015 | 0.017 |
| Common clay drainage tile | 0.011 | 0.012 | 0.014 | 0.017 |
| Glazed brickwork | 0.011 | 0.012 | 0.013 | 0.015 |
| Brick in cement mortar; brick sewers | 0.012 | 0.013 | 0.015 | 0.017 |

In: Metcalf & Eddy, Inc. (George Tchobanoglous). *Wastewater Engineering: Collection and Pumping of Wastewater*. McGraw-Hill, Inc. 1981. (Table 2-1)

Manning's Equation: n Values

| Surface | Best | Good | Fair | Fair |
|-------------------------|-------|-------|-------|-------|
| Neat cement surfaces | 0.010 | 0.011 | 0.012 | 0.013 |
| Cement mortar surfaces | 0.011 | 0.012 | 0.013 | 0.015 |
| Concrete pipe | 0.012 | 0.013 | 0.015 | 0.016 |
| Wood stave pipe | 0.010 | 0.011 | 0.012 | 0.013 |
| Plank flumes | | | | |
| Planed | 0.010 | 0.012 | 0.013 | 0.014 |
| Unplaned | 0.011 | 0.013 | 0.014 | 0.015 |
| With battens | 0.012 | 0.015 | 0.016 | 0.016 |
| Concrete-lined channels | 0.012 | 0.014 | 0.016 | 0.018 |
| Cement-rubble surface | 0.017 | 0.020 | 0.025 | 0.030 |
| Dry-rubble surface | 0.025 | 0.030 | 0.033 | 0.035 |
| Dressed-ashlar surface | 0.013 | 0.014 | 0.015 | 0.017 |

In: Metcalf & Eddy, Inc. (George Tchobanoglous). *Wastewater Engineering: Collection and Pumping of Wastewater*. McGraw-Hill, Inc. 1981. (Table 2-1)

Manning's Equation: n Values

| Surface | Best | Good | Fair | Bad |
|--|--------|--------|--------|-------|
| Semicircular metal flumes, smooth | 0.011 | 0.012 | 0.013 | 0.015 |
| Semicircular metal flumes, corrugated | 0.0225 | 0.025 | 0.0275 | 0.030 |
| Canals and ditches | | | | |
| Earth, straight and uniform | 0.017 | 0.020 | 0.0225 | 0.025 |
| Rock cuts, smooth and uniform | 0.025 | 0.030 | 0.033 | 0.035 |
| Rock cuts, jagged and irregular | 0.035 | 0.040 | 0.045 | 0.045 |
| Dredged-earth channels | 0.025 | 0.0275 | 0.030 | 0.033 |
| Canals, rough stony beds, weeds on earth banks | 0.025 | 0.030 | 0.035 | 0.040 |
| Earth bottom, rubble sides | 0.028 | 0.030 | 0.033 | 0.035 |

In: Metcalf & Eddy, Inc. (George Tchobanoglous). *Wastewater Engineering: Collection and Pumping of Wastewater*. McGraw-Hill, Inc. 1981. (Table 2-1)

Manning's Equation: n Values

| Surface | Best | Good | Fair | Bad |
|--|-------|--------|-------|-------|
| Natural-stream channels | | | | |
| Clean, straight bank, full stage, no rifts/deep pools | 0.025 | 0.0275 | 0.030 | 0.033 |
| Clean, straight bank, full stage, no rifts deep pools, but some weeds/stone | 0.030 | 0.033 | 0.035 | 0.040 |
| Winding, some pools and shoals, clean | 0.033 | 0.035 | 0.040 | 0.045 |
| Winding, some pools/shoals, clean, lower stages, more ineffective slope/sections | 0.040 | 0.045 | 0.050 | 0.055 |
| Winding, some pools/shoals, some weeds/stones | 0.035 | 0.040 | 0.045 | 0.050 |
| Winding, some pools/shoals, clean, lower stages, more ineffective slope/sections, stony sections | 0.045 | 0.050 | 0.055 | 0.060 |
| Sluggish river reaches, weedy or very deep pools | 0.050 | 0.060 | 0.070 | 0.080 |
| Very weedy reaches | 0.075 | 0.100 | 0.125 | 0.150 |

In: Metcalf & Eddy, Inc. (George Tchobanoglous). *Wastewater Engineering: Collection and Pumping of Wastewater*. McGraw-Hill, Inc. 1981. (Table 2-1)

Manning's Equation: n Values

| Nature of Surface | Manning's n Range |
|--------------------------------|-------------------|
| Concrete Pipe | 0.011 – 0.013 |
| Corrugated Metal Pipe | 0.019 – 0.030 |
| Vitrified Clay Pipe | 0.012 – 0.014 |
| Steel Pipe | 0.009 – 0.011 |
| Monolithic Concrete | 0.012 – 0.017 |
| Cement Rubble | 0.017 – 0.025 |
| Brick | 0.014 – 0.017 |
| Laminated Treated Wood | 0.015 – 0.017 |
| Open Channels | |
| Lined with Concrete | 0.013 – 0.022 |
| Earth, clean, after weathering | 0.018 – 0.020 |

In: Viessman and Hammer. *Water Supply and Pollution Control, Sixth Edition*. 1998. (Table 6.1) Adapted from: *Design Charts for Open-Channel Flow*. U.S. Department of Transportation, Federal Highway Administration, Hydraulic Design Series No. 3. U.S. Government Printing Office, Washington, D.C. 1961.

Manning's Equation: n Values

| Nature of Surface | Manning's n Range |
|---|-------------------|
| Open Channels | |
| Earth, with grass and some weeds | 0.025 – 0.030 |
| Excavated in rock, smooth | 0.035 – 0.040 |
| Excavated in rock, jagged and irregular | 0.040 – 0.045 |
| Natural Stream Channels | 0.012 – 0.017 |
| No boulders or brush | 0.028 – 0.033 |
| Dense growth of weeds | 0.035 – 0.050 |
| Bottom of cobbles with large boulders | 0.050 – 0.070 |
| Earth, with grass and some weeds | 0.025 – 0.030 |
| Excavated in rock, smooth | 0.035 – 0.040 |
| Excavated in rock, jagged and irregular | 0.040 – 0.045 |

In: Viessman and Hammer. *Water Supply and Pollution Control, Sixth Edition*. 1998. (Table 6.1) Adapted from: *Design Charts for Open-Channel Flow*. U.S. Department of Transportation, Federal Highway Administration, Hydraulic Design Series No. 3. U.S. Government Printing Office, Washington, D.C. 1961.

Manning's Equation

Example:

- What is the velocity of water in a 1-inch diameter pipe that has a slope of 2%, assuming that the pipe is flowing full?

The roughness coefficient for the pipe = $n = 0.013$.

$S = 2\% = 0.02$

Calculate hydraulic radius, R .

R (pipe full) = $D/4 = [(1 \text{ inch})/(12 \text{ in/ft})]/4 = 0.021 \text{ ft}$

- Substituting into Manning's Equation:

$$V = \frac{1.49}{0.013} (0.021 \text{ ft})^{2/3} (0.02)^{1/2}$$

$$V = 114.6(0.076)(0.1414)$$

$$V = 1.23 \text{ ft/sec}$$

Manning's Equation

Diameter of a Pipe Flowing Full Using Manning's Equation for Velocity

$$V = \frac{1.49}{n} R^{2/3} S^{1/2}$$

$$A = \frac{\pi}{4} D^2$$

$$P = \pi D$$

$$R = \frac{A}{P} = \frac{\frac{\pi}{4} D^2}{\pi D} = \frac{D}{4}$$

Manning's Equation

Diameter of a Pipe Flowing Full Using Manning's Equation for Velocity

$$V = \frac{1.49}{n} \left(\frac{D}{4} \right)^{2/3} S^{1/2}$$

$$\frac{nV}{1.49S^{1/2}} = \left(\frac{D}{4} \right)^{2/3}$$

$$\left(\frac{nV}{1.49S^{1/2}} \right)^{3/2} = \frac{D}{4}$$

$$4 \left(\frac{nV}{1.49S^{1/2}} \right)^{3/2} = D$$

Manning's Equation

- For Fluid Flow in U.S. Customary Units:

$$Q = \frac{1.486AR^{2/3}S^{1/2}}{n}$$

Where
 Q = flow (ft³/sec)
 A = cross-sectional area of flow (ft²)
 R = hydraulic radius (ft)
 S = slope of the energy grade line
 n = Manning's roughness coefficient

Manning's Equation

- For Fluid Flow in SI Units:

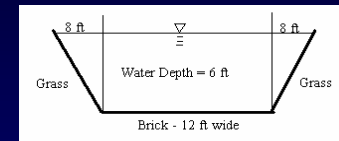
$$Q = \frac{AR^{2/3}S^{1/2}}{n}$$

Where
 Q = flow (m³/sec)
 A = cross-sectional area of flow (m²)
 R = hydraulic radius (m)
 S = slope of the energy grade line
 n = Manning's roughness coefficient

Manning's Equation

Example:

- Determine the discharge of a trapezoidal channel having a brick bottom and grassy sides, with the following dimensions: depth = 6 ft, bottom width = 12 ft, top width = 18 ft. Assume S = 0.002.



- For the rectangular area with the brick bottom:
 $n = 0.017$
 To use Manning's, need A and R:
 $A = (\text{Depth of Flow})(\text{Bottom Width of Channel})$
 $A = (6 \text{ ft})(12 \text{ ft}) = 72 \text{ ft}^2$
 $P = \text{wetted perimeter} = 12 \text{ ft}$
 $R = A/P = 72 \text{ ft}^2/12 \text{ ft} = 6 \text{ ft}$

Manning's Equation

- Substituting into Manning's:

$$Q = \frac{1.49}{0.017} (72 \text{ ft}^2) (6 \text{ ft})^{2/3} (0.002)^{1/2}$$

$$Q = 930.75 \text{ ft}^3/\text{sec}$$

$$Q = 931 \text{ ft}^3/\text{sec}$$

- For the two triangular areas with grass-lined sides:
n = 0.025

To use Manning's, need A and R for one side:

$$A = (0.5)(\text{Depth of Flow})(\text{Width of One Side})$$

$$A = 0.5(6 \text{ ft})(3 \text{ ft}) = 9 \text{ ft}^2$$

Manning's Equation

- To use Manning's, need A and R for one side:
P = hypotenuse of right triangle
 $P^2 = (\text{Depth of Flow})^2 + (\text{Width of One Side})^2$
 $P^2 = (6 \text{ ft})^2 + (3 \text{ ft})^2$
 $P^2 = 36 \text{ ft}^2 + 9 \text{ ft}^2 = 45 \text{ ft}^2$
P = 6.71 ft
R = A/P = 9 ft²/6.71 ft = 1.35 ft

- Substituting into Manning's for one side of the channel:

$$Q = \frac{1.49}{0.025} (9 \text{ ft}^2) (1.35 \text{ ft})^{2/3} (0.002)^{1/2}$$

$$Q = 29.3 \text{ ft}^3/\text{sec}$$

Manning's Equation

Total Flow = Flow from Rectangular Section +
2(Flow from One Triangular Section)

$$\text{Total Flow} = 931 \text{ cfs} + 2(29.3 \text{ cfs}) = 989.6 \text{ cfs}$$

Manning's Equation

- Also can use nomographs to get solution.

From: Warren Viessman, Jr. and Mark Hammer. *Water Supply and Pollution Control Sixth Edition*. Addison-Wesley. 1998.

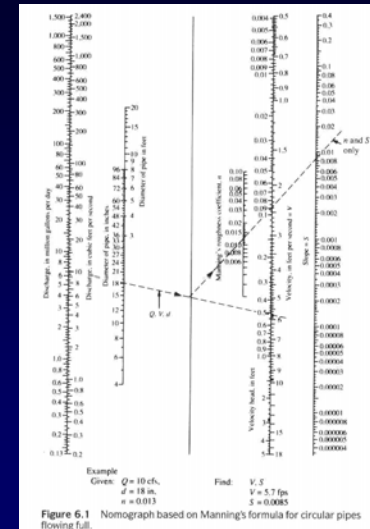


Figure 6.1 Nomograph based on Manning's formula for circular pipes flowing full.

Manning's Equation

- Also can use nomographs to get solution.

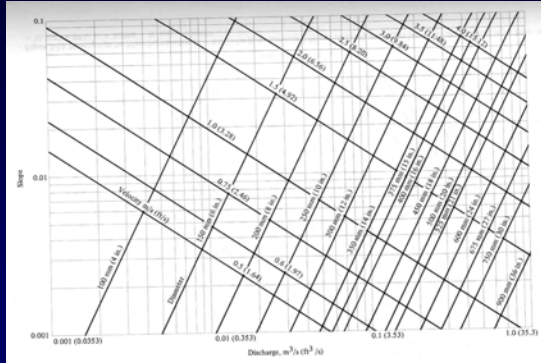


Figure 2-12 Nomograph for Manning equation ($n = 0.013$) for flows between 0.001 and 1.0 m^3/s and slopes between 0.001 and 0.1 m/m. Note: $m^3/s \times 35.3147 = ft^3/s$; $m \times 3.2808 = ft$; $mm \times 0.09937 = in$.

From: Metcalf and Eddy, Inc. and George Tchobanoglous. *Wastewater Engineering: Collection and Pumping of Wastewater*. McGraw-Hill, Inc. 1981.

Manning's Equation

- Also can use nomographs to get solution.

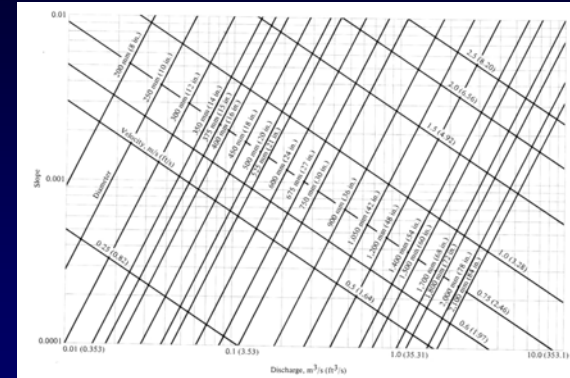


Figure 2-13 Nomograph for Manning equation ($n = 0.013$) for flows between 0.01 and 10.0 m^3/s and slopes between 0.001 and 0.01 m/m. Note: $m^3/s \times 35.3147 = ft^3/s$; $m \times 3.2808 = ft$; $mm \times 0.09937 = in$.

From: Metcalf and Eddy, Inc. and George Tchobanoglous. *Wastewater Engineering: Collection and Pumping of Wastewater*. McGraw-Hill, Inc. 1981.

Manning's Equation

- Also can use nomographs to get solution.

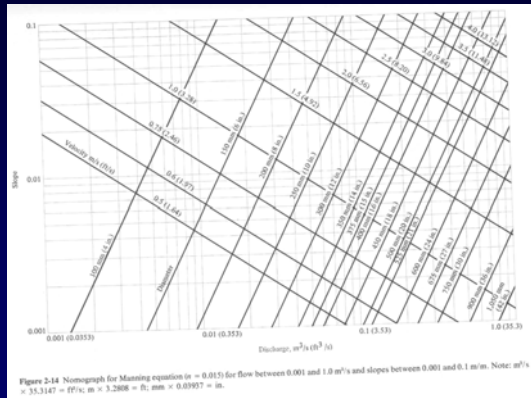


Figure 2-14 Nomograph for Manning equation ($n = 0.013$) for flow between 0.001 and 1.0 m^3/s and slopes between 0.001 and 0.1 m/m. Note: $m^3/s \times 35.3147 = ft^3/s$; $m \times 3.2808 = ft$; $mm \times 0.09937 = in$.

From: Metcalf and Eddy, Inc. and George Tchobanoglous. *Wastewater Engineering: Collection and Pumping of Wastewater*. McGraw-Hill, Inc. 1981.

Manning's Equation

- Also can use nomographs to get solution.

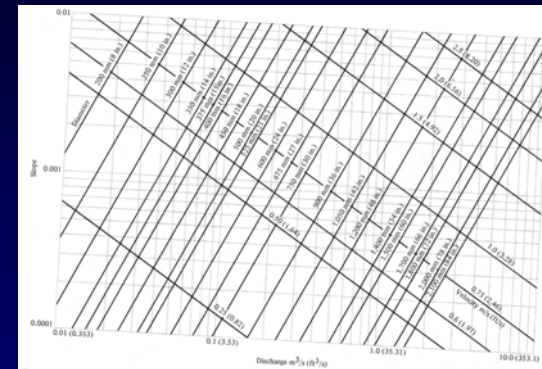


Figure 2-15 Nomograph for Manning equation ($n = 0.013$) for flows between 0.01 and 10.0 m^3/s and slopes between 0.001 and 0.01 m/m. Note: $m^3/s \times 35.3147 = ft^3/s$; $m \times 3.2808 = ft$; $mm \times 0.09937 = in$.

From: Metcalf and Eddy, Inc. and George Tchobanoglous. *Wastewater Engineering: Collection and Pumping of Wastewater*. McGraw-Hill, Inc. 1981.

Manning's Equation

Recall that the diameter of a pipe flowing full using Manning's equation :

$$\left(\frac{4^{5/3} n Q}{1.49 \pi S^{1/2}} \right)^{3/8} = D$$

Manning's Equation

Example:

- Given a 20-inch concrete conduit with a roughness coefficient of $n = 0.013$, $S = 0.005$ and a discharge capacity of 9.85 cfs, what diameter pipe is required to quadruple the capacity.
- Use Manning's equation to solve for pipe diameter:

$$D = \left(\frac{4^{5/3} n Q}{1.49 \pi S^{1/2}} \right)^{3/8}$$

- To quadruple capacity, $Q = 39.4 \text{ ft}^3/\text{sec}$.

Manning's Equation

- Substituting:

$$D = \left(\frac{4^{5/3} (0.013) (39.4 \text{ ft}^3/\text{sec})}{1.49 \pi (0.005)^{1/2}} \right)^{3/8}$$

$$D = 2.8 \text{ ft} = 33.6 \text{ in}$$

- Want smallest commercial pipe size whose ID is greater than or equal to 33.6 in. Use a 36-in. pipe.

Or can be solved by using the nomograms.

- To use SI unit nomograms, need to convert flow rate to SI units:
 $Q = 39.4 \text{ ft}^3/\text{sec} (0.3048 \text{ m/ft})^3 = 1.116 \text{ m}^3/\text{sec} = 1.12 \text{ m}^3/\text{sec}$

Manning's Equation

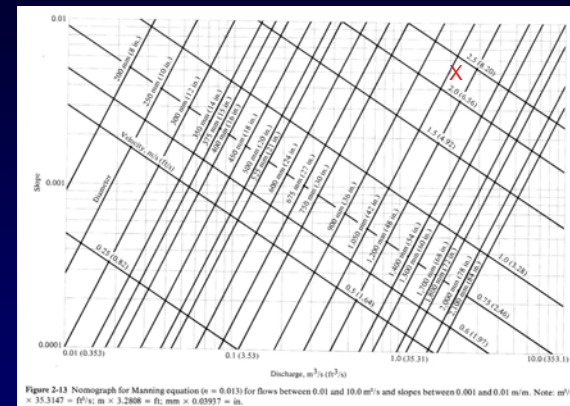


Figure 2-13 Nomograph for Manning equation ($n = 0.013$) for flows between 0.01 and 10.0 m^3/s and slopes between 0.001 and 0.01 m/m . Note: $\text{m}^3/\text{s} = 35.3147 \text{ ft}^3/\text{sec}$; $\text{m} = 3.2808 \text{ ft}$; $\text{mm} = 0.09937 \text{ in}$.

From nomogram, D should be slightly greater than 1050 mm (42 inches). Based on the nomogram, use a 48-in. diameter pipe.

Manning's Equation

Example:

- Determine the head loss in a 46-cm concrete pipe with an average velocity of 1.0 m/sec and a length of 30 m.

- For a pipe flowing full:

$$R = \frac{D}{4} = \frac{0.46m}{4} = 0.115m$$

- By definition: Slope of energy line = Head Loss/Length of Pipe

Or: Head Loss = h_L = (Slope)(Pipe Length)

- Let $n = 0.012$ (concrete pipe)

- Solve Manning's for Slope: $V = \frac{1}{n} R^{2/3} S^{1/2}$

$$S^{1/2} = \frac{nV}{R^{2/3}}$$

$$S = \left(\frac{nV}{R^{2/3}} \right)^2$$

Manning's Equation

- Substituting:

$$S = \left(\frac{0.012(1m/sec)}{0.115^{2/3}} \right)^2$$

$$S = 0.0018$$

- Head Loss = Slope(Pipe Length)

$$h_L = 0.0018(30 m) = 0.054 m$$

- Also can use nomogram to get the slope. For $D = 460$ mm and $V = 1$ m/sec.

$$\text{Slope} = 0.0028$$

$$\text{Head Loss} = \text{Slope}(\text{Pipe Length})$$

$$h_L = 0.0028(30 m) = 0.084 m$$

- Both solution methods show that the head loss is less than 0.10 m.

Manning's Equation

- For $D = 460$ mm (18 in.) and $V = 1$ m/sec (3.3 fps).

$$\text{Slope} = 0.0028$$

$$\text{Head Loss} = \text{Slope}(\text{Pipe Length})$$

$$h_L = 0.0028(30 m) = 0.084 m$$

